

The micromorphic approach to plasticity and phase transformation

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Objectives

The objectives of this presentation are two-fold:

- propose a systematic procedure to extend standard elastoviscoplasticity models to include:
 - ★ size effects in the hardening behaviour of materials (grain size effects...)
 - ★ regularization properties in the softening behaviour (strain localization...)
- unify the “zoology” of generalized continuum models:
 - ★ “Classical” generalized continua: Cosserat, second gradient, micromorphic media (Mindlin, 1964; Eringen and Suhubi, 1964; Mindlin and Eshel, 1968)
 - ★ strain gradient plasticity, “implicit gradient approach” ... (Aifantis, 1987; Fleck and Hutchinson, 2001; Gurtin, 2003; Engelen et al., 2003)
- establish links between generalized continuum mechanics and phase field approaches

Plan

- 1 The micromorphic approach to plasticity
 - Continuum thermomechanics
 - Full micromorphic and microstrain theories
- 2 Microstrain gradient plasticity
 - Gradient of plastic microstrain
 - Consistency condition
 - Anisothermal strain gradient plasticity
- 3 Internal constraint in the micromorphic approach
- 4 Microdiffusion and phase field approach

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State space

- **observable and controllable variables** (temperature, strain...)

$$\{T, \boldsymbol{\varepsilon}\}$$

- **internal degrees of freedom** (controllable variables that account for some aspects of the microstructure)

$$\{\alpha, \nabla\alpha\}$$

they have associated stresses and α or its associated force can be prescribed at the boundary

- **internal variables** are the remembrance of internal degrees of freedom; they cannot be controlled

$$\{\alpha\}$$

The micromorphic approach (1)

- Start from an initial classical elastoviscoplastic model with internal variables

$$DOF0 = \{\underline{\mathbf{u}}\}, \quad STATE0 = \{\underline{\mathbf{F}}, \quad T, \quad \alpha\}$$

- Select one variable $\phi \in STATE0$ and introduce the associated micromorphic variable ${}^x\phi$ as an additional degree of freedom and, possibly, state variable:

$$DOF = \{\underline{\mathbf{u}}, \quad {}^x\phi\}, \quad STATE = \{\underline{\mathbf{F}}, \quad T, \quad \alpha, \quad {}^x\phi, \quad \nabla {}^x\phi\}$$

- Extend the power of internal forces

$$\mathcal{P}^{(i)}(\underline{\mathbf{v}}^*, {}^x\dot{\phi}^*) = - \int_{\mathcal{D}} \rho^{(i)}(\underline{\mathbf{v}}^*, {}^x\dot{\phi}^*) dV$$

$$\rho^{(i)}(\underline{\mathbf{v}}^*, {}^x\dot{\phi}^*) = \underline{\underline{\boldsymbol{\sigma}}} : \nabla \underline{\mathbf{v}}^* + a {}^x\dot{\phi}^* + \underline{\mathbf{b}} \cdot \nabla {}^x\dot{\phi}^*$$

$a, \underline{\mathbf{b}}$ generalized stresses, *microforces* (Gurtin, 1996)

- Derive additional balance equation and boundary conditions

$$\operatorname{div} \underline{\mathbf{b}} - a = 0, \quad \forall \underline{\mathbf{x}} \in \Omega, \quad \underline{\mathbf{b}} \cdot \underline{\mathbf{n}} = a^c, \quad \forall \underline{\mathbf{x}} \in \partial\Omega$$

The micromorphic approach (2)

- More generally, in the presence of volume generalized forces:

$$\operatorname{div}(\underline{\mathbf{b}} - \underline{\mathbf{b}}^e) - a + a^e = 0, \quad \forall \underline{\mathbf{x}} \in \Omega, \quad (\underline{\mathbf{b}} - \underline{\mathbf{b}}^e) \cdot \underline{\mathbf{n}} = a^c, \quad \forall \underline{\mathbf{x}} \in \partial\Omega$$

- Enhance the local balance of energy and the entropy inequality

$$\rho \dot{\epsilon} = p^{(i)} - \operatorname{div} \underline{\mathbf{q}} + \rho r, \quad -\rho(\dot{\psi} + \eta \dot{T}) + p^{(i)} - \frac{\underline{\mathbf{q}}}{T} \cdot \nabla T \geq 0$$

- Consider the constitutive functionals:

$$\psi = \hat{\psi}(\underline{\mathbf{F}}^e, T, \alpha, x\phi, \nabla x\phi), \quad \eta = \hat{\eta}(\underline{\mathbf{F}}^e, T, \alpha, x\phi, \nabla x\phi)$$

$$\underline{\boldsymbol{\sigma}} = \hat{\boldsymbol{\sigma}}(\underline{\mathbf{F}}^e, T, \alpha, x\phi, \nabla x\phi)$$

$$a = \hat{a}(\underline{\mathbf{F}}^e, T, \alpha, x\phi, \nabla x\phi), \quad \underline{\mathbf{b}} = \hat{\underline{\mathbf{b}}}(\underline{\mathbf{F}}^e, T, \alpha, x\phi, \nabla x\phi)$$

- Derive the state laws (Coleman and Noll, 1963)

$$\underline{\boldsymbol{\sigma}} = \rho \frac{\partial \hat{\psi}}{\partial \underline{\mathbf{F}}^e} \cdot \underline{\mathbf{F}}^{eT}, \quad \eta = -\frac{\partial \hat{\psi}}{\partial T}, \quad X = \rho \frac{\partial \hat{\psi}}{\partial \alpha}, \quad a = \frac{\partial \hat{\psi}}{\partial x\phi}, \quad \underline{\mathbf{b}} = \frac{\partial \hat{\psi}}{\partial \nabla x\phi}$$

- Residual dissipation
$$D^{res} = W^p - X\dot{\alpha} - \frac{\underline{\mathbf{q}}}{T} \cdot \nabla T \geq 0$$

The micromorphic approach (3)

- Take a simple quadratic potential

$$\psi(\underline{\mathbf{F}}, T, \alpha, {}^x\phi, \nabla^x\phi) = \psi_1(\underline{\mathbf{F}}, \alpha, T) + \psi_2(\mathbf{e} = \phi - {}^x\phi, \nabla^x\phi, T)$$

$$\rho\psi_2 = \frac{1}{2}H_\chi(\phi - {}^x\phi)^2 + \frac{1}{2}A\nabla^x\phi \cdot \nabla^x\phi$$

$$\mathbf{a} = \rho \frac{\partial\psi}{\partial {}^x\phi} = -H_\chi(\phi - {}^x\phi), \quad \underline{\mathbf{b}} = \rho \frac{\partial\psi}{\partial \nabla^x\phi} = A\nabla^x\phi$$

- Simple form of the partial differential equation (homogeneous, isothermal...)

$$\mathbf{a} = \operatorname{div} \underline{\mathbf{b}} \implies {}^x\phi - \frac{A}{H_\chi} \Delta^x\phi = \phi$$

Helmholtz equation with a minus sign and a source term

- Coupling modulus H_χ and characteristic length of the medium

$$l_c^2 = \frac{A}{H_\chi}$$

Stability

$$H_\chi > 0, \quad A > 0$$

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Micromorphic continuum

Micromorphic continuum according to (Eringen and Suhubi, 1964; Mindlin, 1964)

- Select variable:

$$\phi \equiv \underline{\underline{\mathbf{F}}}, \quad \chi \phi \equiv \underline{\underline{\chi}}$$

$$\rho^{(i)} = \underline{\underline{\boldsymbol{\sigma}}} : \underline{\underline{\nabla \dot{\mathbf{u}}}} + \underline{\underline{\mathbf{a}}} : \underline{\underline{\dot{\chi}}} + \underline{\underline{\mathbf{B}}} : \underline{\underline{\nabla \dot{\chi}}}$$

- application of the principle of (infinitesimal) material frame indifference, (infinitesimal) change of observer of rate $\underline{\underline{\mathbf{w}}}$:

$$\underline{\underline{\nabla \dot{\mathbf{u}}}} \implies \underline{\underline{\nabla \dot{\mathbf{u}}}} + \underline{\underline{\mathbf{w}}}, \quad \underline{\underline{\dot{\chi}}} \implies \underline{\underline{\dot{\chi}}} + \underline{\underline{\mathbf{w}}}$$

$\implies \underline{\underline{\boldsymbol{\sigma}}} + \underline{\underline{\mathbf{a}}}$ must be symmetric. Rewrite the virtual power:

$$\rho^{(i)} = \underline{\underline{\boldsymbol{\sigma}}} : \underline{\underline{\dot{\boldsymbol{\varepsilon}}}} + \underline{\underline{\mathbf{s}}} : (\underline{\underline{\nabla \dot{\mathbf{u}}}} - \underline{\underline{\dot{\chi}}}) + \underline{\underline{\mathbf{S}}} : \underline{\underline{\nabla \dot{\chi}}}$$

- two balance equations:

$$\operatorname{div} (\underline{\underline{\boldsymbol{\sigma}}} + \underline{\underline{\mathbf{s}}}) + \rho \underline{\underline{\mathbf{f}}} = 0, \quad \operatorname{div} \underline{\underline{\mathbf{S}}} + \underline{\underline{s}} = 0$$

Microstrain continuum

Microstrain continuum after (Forest and Sievert, 2006)

- Select

$$\phi \equiv \underset{\sim}{\mathbf{C}} = \underset{\sim}{\mathbf{F}}^T \cdot \underset{\sim}{\mathbf{F}}, \quad {}^x\phi \equiv {}^x\underset{\sim}{\mathbf{C}}, \quad \text{or} \quad \phi \equiv \underset{\sim}{\boldsymbol{\varepsilon}}, \quad {}^x\phi \equiv {}^x\underset{\sim}{\boldsymbol{\varepsilon}}$$

$$p^{(i)} = \underset{\sim}{\boldsymbol{\sigma}} : \dot{\underset{\sim}{\boldsymbol{\varepsilon}}} + \underset{\sim}{\mathbf{a}} : {}^x\dot{\underset{\sim}{\boldsymbol{\varepsilon}}} + \underset{\sim}{\mathbf{b}} : \nabla^x \underset{\sim}{\boldsymbol{\varepsilon}}$$

- Constitutive coupling between macro and microstrain via the relative strain

$$\underset{\sim}{\mathbf{e}} := \underset{\sim}{\boldsymbol{\varepsilon}} - {}^x\underset{\sim}{\boldsymbol{\varepsilon}}$$

$$\psi(\underset{\sim}{\boldsymbol{\varepsilon}}^e, T, \alpha, \underset{\sim}{\mathbf{e}} := \underset{\sim}{\boldsymbol{\varepsilon}} - {}^x\underset{\sim}{\boldsymbol{\varepsilon}}, \underset{\sim}{\mathbf{K}} := \nabla^x \underset{\sim}{\boldsymbol{\varepsilon}})$$

- Take a quadratic potential

$$\underset{\sim}{\mathbf{a}} = H_\chi \underset{\sim}{\mathbf{e}}, \quad \underset{\sim}{\mathbf{b}} = A \nabla^x \underset{\sim}{\boldsymbol{\varepsilon}}$$

- Extra-balance equation

$${}^x\underset{\sim}{\boldsymbol{\varepsilon}} - l_c^2 \Delta^x \underset{\sim}{\boldsymbol{\varepsilon}} = \underset{\sim}{\boldsymbol{\varepsilon}}, \quad \text{with} \quad l_c^2 = \frac{A}{H_\chi}$$

example: microfoams

(Dillard et al., 2006)

Cosserat continuum

Cosserat continuum

$$\phi = \mathbf{R}, \quad {}^x\phi \equiv {}^x\mathbf{R}$$

$$p^{(i)} = \underline{\underline{\sigma}}^s : \underline{\underline{\dot{\epsilon}}} - \underline{\underline{\sigma}}^a : ((\nabla \underline{\underline{\dot{u}}})^a - \underline{\underline{\dot{R}}}\cdot\underline{\underline{R}}^T) + \underline{\underline{M}} : \underline{\underline{\dot{\kappa}}}$$

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General scalar microstrain gradient plasticity

- Classical and generalized plasticity

$$DOF0 = \{\underline{\mathbf{u}}\} \quad STATE0 = \{\underline{\boldsymbol{\varepsilon}}^e, \quad p, \quad \alpha\}$$

$$\phi \equiv p, \quad {}^x\phi \equiv {}^x p$$

$$DOF = \{\underline{\mathbf{u}}, \quad {}^x p\} \quad STATE = \{\underline{\boldsymbol{\varepsilon}}^e, \quad p, \quad \alpha, \quad {}^x p, \quad \nabla^x p\}$$

- Extra balance equation

$$\rho^{(i)} = \underline{\boldsymbol{\sigma}} : \underline{\dot{\boldsymbol{\varepsilon}}} + a {}^x \dot{p} + \underline{\mathbf{b}} \cdot \nabla^x \dot{p}, \quad \rho^{(c)} = \underline{\mathbf{t}} \cdot \underline{\dot{\mathbf{u}}} + a^c {}^x \dot{p}$$

$$\operatorname{div} \underline{\mathbf{b}} - a = 0, \quad \forall \underline{\mathbf{x}} \in \Omega, \quad \underline{\mathbf{b}} \cdot \underline{\mathbf{n}} = a^c, \quad \forall \underline{\mathbf{x}} \in \partial\Omega$$

- State laws

$$\underline{\boldsymbol{\varepsilon}} = \underline{\boldsymbol{\varepsilon}}^e + \underline{\boldsymbol{\varepsilon}}^p$$

$$\underline{\boldsymbol{\sigma}} = \rho \frac{\partial \psi}{\partial \underline{\boldsymbol{\varepsilon}}^e}, \quad R = \rho \frac{\partial \psi}{\partial p}, \quad X = \rho \frac{\partial \psi}{\partial \alpha}, \quad a = \rho \frac{\partial \psi}{\partial {}^x p}, \quad \underline{\mathbf{b}} = \rho \frac{\partial \psi}{\partial \nabla^x p}$$

- Evolution laws

$$D^{res} = \underline{\boldsymbol{\sigma}} : \underline{\dot{\boldsymbol{\varepsilon}}}^p - R \dot{p} - X \dot{\alpha} \geq 0$$

$$\underline{\dot{\boldsymbol{\varepsilon}}}^p = \dot{\lambda} \frac{\partial f}{\partial \underline{\boldsymbol{\sigma}}}, \quad \dot{p} = -\dot{\lambda} \frac{\partial f}{\partial R}, \quad \dot{\alpha} = -\dot{\lambda} \frac{\partial f}{\partial X}$$

Simplified scalar microstrain gradient plasticity

- Quadratic free energy potential

$$\rho\psi(\underline{\underline{\varepsilon}}^e, p, {}^x p, \nabla^x p) = \frac{1}{2} \underline{\underline{\varepsilon}}^e : \underline{\underline{\Lambda}} : \underline{\underline{\varepsilon}}^e + \frac{1}{2} H p^2 + \frac{1}{2} H_\chi (p - {}^x p)^2 + \frac{1}{2} \nabla^x p \cdot \underline{\underline{\mathbf{A}}} \cdot \nabla^x p$$

- Constitutive equations

$$\underline{\underline{\sigma}} = \underline{\underline{\Lambda}} : \underline{\underline{\varepsilon}}^e, \quad a = -H_\chi (p - {}^x p), \quad \underline{\underline{\mathbf{b}}} = \underline{\underline{\mathbf{A}}} \cdot \nabla^x p, \quad R = (H + H_\chi) p - H_\chi {}^x p$$

- Substitution of constitutive equation into extra balance equation

$${}^x p - \frac{1}{H_\chi} \operatorname{div} (\underline{\underline{\mathbf{A}}} \cdot \nabla^x p) = p$$

- Homogeneous and isotropic materials

$$\underline{\underline{\mathbf{A}}} = A \underline{\underline{\mathbf{1}}}$$

$${}^x p - \frac{A}{H_\chi} \Delta^x p = p, \quad \text{b.c.} \quad \nabla^x p \cdot \underline{\underline{\mathbf{n}}} = a^c$$

same partial differential equation as in the *implicit gradient-enhanced elastoplasticity* with $a^c = 0$
(Engelen et al., 2003)

Link to Aifantis strain gradient plasticity

- Yield function

$$f(\underline{\sigma}, R) = \sigma_{eq} - \sigma_Y - R$$

- Hardening law

$$R = \frac{\partial \psi}{\partial p} = (H + H_\chi)p - H_\chi^\chi p$$

- Under plastic loading

$$\sigma_{eq} = \sigma_Y + H^\chi p - A\left(1 + \frac{H}{H_\chi}\right)\Delta^\chi p$$

compare with Aifantis model (Aifantis, 1987)

$$\sigma_{eq} = \sigma_Y + R(p) - c^2 \Delta p$$

The equivalence is obtained for $H_\chi = \infty$ (internal constraint):

$${}^\chi p \simeq p, \quad A = c^2$$

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Consistency condition

- Consistency condition

$$\begin{aligned}\dot{f} &= \frac{\partial f}{\partial \boldsymbol{\sigma}} : \dot{\boldsymbol{\sigma}} + \frac{\partial f}{\partial R} \dot{R} \\ &= \frac{\partial \sigma_{eq}}{\partial \boldsymbol{\sigma}} : \boldsymbol{\Lambda} : (\dot{\boldsymbol{\varepsilon}} - \dot{\boldsymbol{\varepsilon}}^p) - \frac{\partial R}{\partial p} \dot{p} - \frac{\partial R}{\partial x_p} {}^x\dot{p} = 0\end{aligned}$$

- Plastic multiplier

$$\dot{p} = \frac{\boldsymbol{N} : \boldsymbol{\Lambda} : \dot{\boldsymbol{\varepsilon}} - \frac{\partial R}{\partial x_p} {}^x\dot{p}}{\boldsymbol{N} : \boldsymbol{\Lambda} : \boldsymbol{N} + \frac{\partial R}{\partial p}}, \quad \text{with} \quad \boldsymbol{N} = \frac{\partial \sigma_{eq}}{\partial \boldsymbol{\sigma}}$$

where $\dot{\boldsymbol{\varepsilon}}$ and ${}^x\dot{p}$ are controllable variable.

- Even though the yield condition can be written as a partial differential equation, there is no need for a variational formulation of the consistency condition contrary to (Mühlhaus and Aifantis, 1991; Liebe et al., 2001). There is no need for a plastic front tracking technique. The plastic microstrain ${}^x p$ and the generalized traction $\boldsymbol{b} \cdot \boldsymbol{n}$ are continuous across the elastic/plastic domain.

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Thermal effects

- For temperature dependent parameters

$$a = \operatorname{div} \underline{\mathbf{b}} = \operatorname{div} (A \nabla^x p) = A \Delta^x p + \frac{\partial A}{\partial T} \nabla T \cdot \nabla^x p$$

$${}^x p - \frac{A}{H_x} \Delta^x p - \frac{1}{H_x} \frac{\partial A}{\partial T} \nabla T \cdot \nabla^x p = p$$

- Consistency condition

$$\dot{p} = \frac{\underline{\mathbf{N}} : \underline{\underline{\Lambda}} : (\underline{\dot{\underline{\epsilon}}} - \underline{\dot{\underline{\epsilon}}}^{th}) - \frac{\partial R}{\partial x p} {}^x \dot{p} - \frac{\partial R}{\partial T} \dot{T}}{\underline{\mathbf{N}} : \underline{\underline{\Lambda}} : \underline{\mathbf{N}} + \frac{\partial R}{\partial p}}$$

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Internal constraint and gradient of internal variable approach

- Impose the internal constraint that

$${}^x\phi \simeq \phi \implies \underline{\mathbf{K}} \simeq \nabla\phi$$

Then, the generalized stress a becomes a Lagrange multiplier.

- Examples

- ★ $\phi \equiv \underline{\mathbf{F}}$ second gradient model (Mindlin, 1965)
- ★ $\phi \equiv \underline{\mathbf{p}}$ Aifantis model (Aifantis, 1987; Fleck and Hutchinson, 2001)
- ★ $\phi \equiv \underline{\underline{\boldsymbol{\varepsilon}}}^p$ strain gradient plasticity (Forest and Sievert, 2003; Gurtin, 2003)

$$\rho^{(i)} = \underline{\boldsymbol{\sigma}} : \underline{\underline{\boldsymbol{\varepsilon}}}^e + \underline{\mathbf{s}} : \underline{\underline{\boldsymbol{\varepsilon}}}^p + \underline{\underline{\mathbf{S}}} : \underline{\underline{\boldsymbol{\varepsilon}}}^p, \quad \text{div } \underline{\underline{\mathbf{S}}} = \underline{\mathbf{s}} - \underline{\boldsymbol{\sigma}}^{dev}$$

The yield condition becomes a PDE (Aifantis, Fleck–Hutchinson, Gurtin):

$$\sigma_{eq} = \sigma_Y + Hp - A\Delta p$$

What does the yield criterion become?

- What do the boundary conditions become?
 - ★ For the second gradient theory, intricate b.c. involving surface curvature
 - ★ For gradient of plastic strain, $\underline{\underline{\mathbf{S}}}\cdot\underline{\mathbf{n}} = \underline{\mathbf{m}}$

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Microdiffusion (1)

Putting Geers' approach of viscoplasticity and Cahn–Hilliard diffusion within the micromorphic framework (Ubachs et al., 2004)

- Mass concentration and microconcentration

$$\phi \equiv c, \quad {}^x\phi \equiv {}^x c, \quad STATE = \{c, {}^x c, \nabla {}^x c\}$$

- Additional power due to microdiffusion (compare: there is no power produced by classical diffusion!)

$$p^{(i)} = a {}^x \dot{c} + \underline{\mathbf{b}} \cdot \nabla {}^x \dot{c}, \quad a = \operatorname{div} \underline{\mathbf{b}}, \quad \underline{\mathbf{b}} \cdot \underline{\mathbf{n}} = a^c$$

in addition to the balance of mass:

$$\rho \dot{c} = -\operatorname{div} \underline{\mathbf{J}}$$

- First and second principles (isothermal for brevity)

$$\rho \dot{\epsilon} = p^{(i)}, \quad \int_V \rho \dot{\eta} dV \geq \int_V \frac{\mu \underline{\mathbf{J}}}{T} dS$$

mass flux $\underline{\mathbf{J}}$ and chemical potential μ

$$\rho T \dot{\eta} - \operatorname{div} (\mu \underline{\mathbf{J}}) \geq 0; \quad -\rho \dot{\psi} + p^{(i)} - \operatorname{div} (\mu \underline{\mathbf{J}}) \geq 0$$

Microdiffusion (2)

- State laws $\rho\psi(c, x_c, \nabla x_c)$

$$(a - \rho \frac{\partial \psi}{\partial x_c}) \dot{x}_c + (\underline{\mathbf{b}} - \rho \frac{\partial \psi}{\partial \nabla x_c}) \cdot \nabla x_c \dot{c} + \rho (\mu - \frac{\partial \psi}{\partial c}) \dot{c} - \underline{\mathbf{J}} \cdot \nabla \mu \geq 0$$

$$a = \rho \frac{\partial \psi}{\partial x_c}, \quad \underline{\mathbf{b}} = \rho \frac{\partial \psi}{\partial \nabla x_c}, \quad \mu = \frac{\partial \psi}{\partial c}$$

- Quadratic potential

$$\rho\psi = \rho\psi_0(c) + \frac{1}{2} H_x (c - x_c)^2 + \frac{1}{2} \alpha \nabla x_c \cdot \nabla x_c$$

$$a = -H_x (c - x_c) = \operatorname{div} \underline{\mathbf{b}} = \alpha \Delta x_c$$

$$x_c - \lambda^2 \Delta x_c = c, \quad \lambda^2 = \frac{\alpha}{H_x}$$

$$\mu = \rho \frac{\partial \psi_0}{\partial c} + H_x (c - x_c)$$

Relation to Cahn–Hilliard theory

- Mass concentration $\phi \equiv c$, $STATE = \{c, \nabla c\}$

$$\rho^{(i)} = a\dot{c} + \underline{\mathbf{b}} \cdot \nabla \dot{c}, \quad a = \operatorname{div} \underline{\mathbf{b}}, \quad \underline{\mathbf{b}} \cdot \underline{\mathbf{n}} = a^c$$

in addition to the balance of mass $\rho\dot{c} = -\operatorname{div} \underline{\mathbf{J}}$ (Gurtin, 1996)

- First and second principles (isothermal for brevity) $\rho\psi(c, \nabla c)$

$$\rho\dot{\epsilon} = \rho^{(i)}, \quad -\rho\dot{\psi} + \rho^{(i)} - \operatorname{div}(\mu\underline{\mathbf{J}}) \geq 0$$

$$(a + \mu - \rho \frac{\partial \psi}{\partial c})\dot{c} + (\underline{\mathbf{b}} - \rho \frac{\partial \psi}{\partial \nabla c}) \cdot \nabla \dot{c} - \underline{\mathbf{J}} \cdot \nabla \mu \geq 0$$

$$\mu = \rho \frac{\partial \psi}{\partial c} - a, \quad \underline{\mathbf{b}} = \rho \frac{\partial \psi}{\partial \nabla c}$$

- Fick's law $\underline{\mathbf{J}} = -\kappa \nabla \mu$
- Quadratic potential $\rho\psi = \rho\psi_0(c) + \frac{1}{2}\alpha \nabla c \cdot \nabla c$ (Cahn and Hilliard, 1958)

$$\mu = \rho \frac{\partial \psi}{\partial c} - a = \rho \frac{\partial \psi}{\partial c} - \operatorname{div} \underline{\mathbf{b}} = \rho \frac{\partial \psi}{\partial c} - \alpha \Delta c$$

$$\rho\dot{c} = -\operatorname{div} \underline{\mathbf{J}} = \kappa \Delta \mu = \kappa \Delta (\rho \frac{\partial \psi}{\partial c} - \alpha \Delta c)$$

- Equivalence obtained for ${}^x c \simeq c$

$$\rho\dot{c} = \operatorname{div} \nabla \mu = \kappa \Delta (\rho \frac{\partial \psi_0}{\partial c} + H_x(c - {}^x c)) = \kappa \Delta (\rho \frac{\partial \psi_0}{\partial c} - \alpha \Delta {}^x c)$$

Phase field approach (1)

The phase field model as presented by (Gurtin, 1996) falls in the micromorphic approach. There are however two differences compared to the previous examples: $\phi \notin STATE0$, there is a dissipative part associated with $\dot{\phi}$

- Order parameter ϕ as additional degree of freedom in addition to mass concentration; Gurtin assumes that there is a power expenditure by variation of order parameter and its gradient (in contrast to diffusion!)

$$STATE = \{c, \phi, \nabla\phi\}, \quad \rho^{(i)} = a\dot{\phi} + \underline{\mathbf{b}} \cdot \nabla\dot{\phi}$$

- Balance of mass, generalized momentum (no volume forces) and energy

$$\rho\dot{c} = -\operatorname{div} \underline{\mathbf{J}}, \quad \operatorname{div} \underline{\mathbf{b}} - a = 0, \quad \rho\dot{\epsilon} = \rho^{(i)}$$

- Exploitation of second principle *à la* Coleman–Noll

$$\rho^{(i)} - \rho\dot{\psi} - \operatorname{div} \mu \underline{\mathbf{J}} \geq 0$$

Phase field approach (2)

- Exploitation of the second principle (continued)

$$\rho\left(\mu - \frac{\partial\psi}{\partial c}\right)\dot{c} + \left(a - \rho\frac{\partial\psi}{\partial\phi}\right)\dot{\phi} - \left(\underline{\mathbf{b}} - \rho\frac{\partial\psi}{\partial\nabla\phi}\right) \cdot \nabla\dot{\phi} - \underline{\mathbf{J}} \cdot \nabla\mu \geq 0$$

$$\rho\psi = \rho\psi_0(c, \phi) + \frac{1}{2}\alpha\nabla\phi \cdot \nabla\phi, \quad \mu = \frac{\partial\psi}{\partial c} =, \quad \underline{\mathbf{b}} = \rho\frac{\partial\psi}{\partial\nabla\phi}$$

- Accept the dependence $a(c, \phi, \nabla\phi, \dot{\phi})$ and choose the dissipation potential $a^{\text{dis}} = a - \rho\frac{\partial\psi}{\partial\phi}$

$$\Omega(\nabla\mu, a^{\text{dis}}) = \frac{1}{2}\kappa\nabla\mu \cdot \nabla\mu + \frac{1}{2\beta}(a^{\text{dis}})^2$$

$$\underline{\mathbf{J}} = -\frac{\partial\Omega}{\partial\nabla\mu} = -\kappa\nabla\mu, \quad \dot{\phi} = \frac{\partial\Omega}{\partial a^{\text{dis}}} = \frac{1}{\beta}a^{\text{dis}}$$

- Ginzburg–Landau (Allen–Cahn) equation

$$\beta\dot{\phi} = a^{\text{dis}} = a - \rho\frac{\partial\psi_0}{\partial\phi} = \text{div}\underline{\mathbf{b}} - \rho\frac{\partial\psi_0}{\partial\phi} = \alpha\Delta\phi - \rho\frac{\partial\psi_0}{\partial\phi}$$

implemented in this way by Kais Ammar (2007)

Conclusions

Why the name “micromorphic approach”?

- additional degrees of freedom, generally “strain-like” variables, in the spirit of the full micromorphic continuum by Mindlin and Eringen
- coupling of macro and micro-quantities through a dependence of the free energy on a relative strain measure $e = \phi - \chi\phi$
- additional balance equations taking the form of a Helmholtz equation with source term for a simple choice of the free energy function
- constrained micromorphic media: strain gradient plasticity and damage
- microdiffusion model that can be reduced to Cahn-Hilliard model
- applications: finite element simulations of cell-size effects in metallic foams, Cosserat crystal plasticity, micromorphic crystal cleavage fracture...

(Forest et al., 2000; Dillard et al., 2006; Zeghadi et al., 2007)

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